## Errata

| \# | Page | Correction |
| :---: | :---: | :---: |
| 1 | xii, line -10 | resulta en el un buen ajuste |
| 2 | xxii - Figure 56 | Replace FCWR by FCGR |
| 3 | xxii - Figure 58 | Replace CWR by CGR |
| 4 | xxv - Figure 106 | Replace FCW by FCG |
| 5 | $\begin{aligned} & \text { xxv - Figure } \\ & 108 \end{aligned}$ | Replace FCW by FCG |
| 6 | xxvii | Replace FCW by FCG |
| 7 | xxvii | Replace FCWR by FCGR |
| 8 | xxx, line -12 |  |
| 9 | 56, line -8 | synthetic ropes for a given characteristic strength |
| 10 | 56, line -14 | which are shown in Figure 12 |
| 11 | 58 | Replace: Kg By: kg |
| 12 | 60, line - 16 | The equilibrium between the content of chromium (Cr), nickel (Ni), and molybdenum (Mo) is key to improve the hardenability, necessary to guarantee the formation of bainitic structures in large diameter, high-strength mooring chains. |
| 13 | 62, line - 8 | Replace: the other that it is fixed By: the other, which is fixed |
| 14 | 67, line - 14 | Replace: the time consumed by stages II and III depend By: the time consumed by stages I and II depends |
| 15 | 74, equation 8 | Replace: $\frac{\sigma_{a}}{\sigma_{a r}}+\left(\frac{\sigma_{m}}{\sigma_{y}}\right)^{2}=1 \quad$ By: $\quad \frac{\sigma_{a}}{\sigma_{a r}}+\frac{\sigma_{m}}{\sigma_{y}}=1$ |
| 16 | 75, line - 11 | Replace: many test By: many tests |
| 17 | 75, equation 11 | Replace: $\gamma=-0.0002 \sigma_{u}-0.8818$ By: $\gamma=-0.0002 \sigma_{u}+0.8818$ |
| 18 | 76, line - 17 | Replace: There is formulae By: There are formulae |
| 19 | 83, line - 6 | Replace: Figure 13, shows By: Figure 13 shows |
| 20 | 86, line 15,16 | Replace in Figure 39 By: in Figures 38 and 39 |
| 21 | 96, line - 1 | Replace (CWR) By: (CGR) |
| 22 | 96, Figure 48 | Replace da/dN By: da/dt |
| 23 | 96, line - 6 | Replace rate da/dN By: rate da/dt |
| 9 | 96 , line -14 | The higher the strength of the steel, the higher is the susceptibility to SCC, and hence the lower is the $K_{I S C C}$. |
| 24 | 101, Fig. 56 caption | Replace: FCWR By: FCGR |
| 25 | 102, line - 22 | Replace: FCWR By: FCGR |
| 26 | 104, line - 5 | Replace: the two the two graphics By: the two graphics |
| 27 | 104, Fig. 58 caption | Replace: CWR By: CGR |
| 28 | 105, line - 10 | Replace: CWR By: CGR |
| 29 | 109, line - 11 | Replace: studless chain were By: studless chains were |
| 30 | 113, line - 29 | Replace: FCWR By: FCGR |
| 31 | 115, line - 11 | Replace: This trend has been also observed By: This trend has also been observed |
| 32 | 123, Figure 77 caption | Replace: 6-link By: 6 links |


| 33 | 121, line - 7 | Replace: family of curves are derived By: a family of curves is derived |
| :---: | :---: | :---: |
| 34 | 123, line - 17 | Replace: mean value of $\log a \quad$ By: mean value of $a$ |
| 35 | 126, line -17 | Among all, the SWT correction seems to give |
| 36 | 127, line -6 | Corrected fitted lines at different at different mean loads |
| 37 | 127, table 14 | Replace: $7.479 \times 10^{11}$ By: $7.464 \times 10^{11}$ |
| 38 | 130, line 3 | Between the logarithm of the intercept parameter |
| 39 | 143, equation (31) | Replace: Kp By: kp |
| 40 | 146, line - 9 | Replace: plain strain By: plane strain |
| 41 | 147, line - 23 | Replace: later By: latter |
| 42 | $\text { 148, Fig. } 96$ <br> caption | Replace link with semi-elliptical a crack, $\mathrm{a} / \mathrm{d}=0.3$ <br> By: link with a semi elliptical crack, $\mathrm{a} / \mathrm{b}=0.5, \mathrm{a} / \mathrm{d}=0.3$ |
| 43 | 155, line - 8 | Replace: Selected By: selected |
| 44 | 155, line - 15 | Replace: FCWR By: FCGR |
| 45 | 155, Table 20 | Replace: FCWR By: FCGR <br> Replace: FCW By: FCG |
| 46 | 155, Table 21 | Replace: FCWR By: FCGR <br> Replace: FCW By: FCG |
| 47 | $\text { 156, Fig. } 106$ <br> caption | Replace: FCW By: FCG |
| 48 | 156, Fig. 108 caption | Replace: FCW By: FCG |
| 49 | 172, line - 6 | Replace: Carkberg By: Carlberg |
| 50 | 174, Ref. 102 | Replace: threw by three |

