

30 **Abstract**

31 Since polyol is one of the major components in polyurethane foam synthesis, introducing
32 renewably sourced polyols in the foam formulation leads to materials with high renewable
33 carbon content. A series of flexible polyurethane foams with variations in polyol
34 composition were synthesized with castor oil based Lupranol Balance® 50 polyether
35 polyol and corn based polytrimethylene ether glycol mixtures. Water was used as the
36 unique and eco-friendly blowing agent. The effect of the relative amount of each polyol
37 on the structure and properties was analyzed by optical microscopy, Fourier transform
38 infrared spectroscopy, thermogravimetric analysis, tensile and compressive tests,
39 dynamic mechanical analysis and atomic force microscopy. The average molecular
40 weight and hydroxyl number of the polyol components showed to influence the foaming
41 reaction and hence the structure and properties of the polyurethane foam. The newly
42 developed Peak Force Quantitative Nano-Mechanics technique was used to map the
43 elastic modulus values of foam cell struts and it seemed to be adequate to assess the purity
44 of the different phases.

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46 Keywords: Microphase separation, AFM, Peak Force Quantitative Nanomechanics,
47 Vegetable oil based polyols, flexible polyurethane foam

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60 1. INTRODUCTION

61 Flexible polyurethane foams have been widely used in many applications such as
62 mattresses, seating and car industry and they are gaining great interest in areas such as
63 biomedicine, intelligent materials and nanocomposites (Hodlur et al., 2014; Kang et al.,
64 2010; Liu et al., 2013; Singhal et al., 2014). Nowadays, there is a growing concern about
65 environmental issues in material synthesis. This reason together with crude price
66 fluctuations have encouraged scientific community to develop materials, including
67 polyurethanes, based on renewable resources which do not depend on petroleum based
68 raw materials (Rashmi et al., 2013). Regarding renewable-based resources, vegetable oils
69 have received special attention as raw materials for polyol synthesis (Ionescu et al., 2012;
70 Narine et al., 2007; Palanisamy et al., 2011; Sharma et al., 2014). Helling et al., 2009
71 carried out a life cycle assessment analysis for vegetable oil based polyols and
72 demonstrated that a reduction of 33% to 64% on fossil resources consumption as well as
73 a lowering on greenhouse gas emissions could be achievable by using soy or castor oil.

74 Foam synthesis involves two main reactions: blowing and gelling. Blowing reaction
75 arises from the reaction of an isocyanate group with water and yields urea and carbon
76 dioxide, which expands the air bubbles entrapped inside the reactive mixture. Gelling
77 reaction implies an isocyanate group and a hydroxyl group to form a urethane linkage.
78 The microstructure is accepted to be composed by both physical and chemical crosslinks.
79 Physical crosslinks arise when urea groups of sufficient size and concentration establish
80 hydrogen bonding interactions with other urea groups and phase separate from soft
81 segments into hard domains (Dounis et al., 1997). Chemical crosslinks are the result of
82 the urethane reaction, whereby a covalent network is formed between polyurea oligomers
83 and polyol soft segments through urethane bonds. The microstructure and morphology
84 depend on several factors such as the competition between the two main reactions,
85 mobility of urea groups, the level of crosslinks arised from the reaction between the
86 diisocyanate and polyol and the specific interactions between polyol and polyurea
87 segments (Heintz et al., 2005; Li et al., 2002).

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89 Determining the mechanical properties on the micro-and nanoscale is a matter of interest
90 in materials property analysis. Nanoindentation techniques are widely used to assess local
91 mechanical properties. However, this method is time consuming and presents various
92 uncertainties when determining the local elastic modulus (Miller et al., 2008; Varam et

93 al., 2014). When working with soft materials such as polymers, the high deformations
 94 produced in the material and the importance of adhesive forces are important challenges
 95 when using nanoindentation analysis (Gupta et al., 2007; Kohn et al., 2013;
 96 VanLandingham et al., 2011). Peak Force Quantitative Nano-Mechanics is a new
 97 technique that allows the mapping of mechanical properties by using a scanning probe
 98 microscope at a similar scanning speed to Tapping Mode. With difference to Tapping
 99 Mode atomic force microscopy, the controlled variable is the maximum force (Peak
 100 Force) applied to the surface and it is maintained constant during the scan. Force vs
 101 separation curves are obtained and information about adhesion force, elastic modulus,
 102 deformation and dissipation can be extracted (Adamcik et al., 2011). The reduced elastic
 103 modulus can be determined by using the Derjaguin-Muller-Toporov (DMT) model shown
 104 in Eq. (1) (Derjaguin et al., 1975).

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$$106 \quad F_{interaction} = 4/3E^*\sqrt{R(d - d_0)^3} \quad (\text{Eq. 1})$$

107

108 Where $F_{interaction}$ is the tip-sample force, E^* is the reduced elastic modulus, R is the tip
 109 radius and $d - d_0$ is sample deformation.

110 The reduced modulus is related to the sample modulus by Eq. (2).

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$$112 \quad E^* = \left[\frac{1-\nu_s^2}{E_s} + \frac{1-\nu_{tip}^2}{E_{tip}} \right]^{-1} \quad (\text{Eq. 2})$$

113

114 Where E^* is the reduced elastic modulus, ν_s and ν_{tip} are the Poisson's ratios of sample
 115 and tip respectively and E_s and E_{tip} are the elastic modulus of sample and tip
 116 respectively. Considering that E_{tip} is much higher, sample Young's modulus (E_s) can be
 117 calculated if ν_s is known (Pittenger et al., 2012).

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119 The aim of this work was to synthesize flexible polyurethane foams using bio-derived
 120 polyols and to analyze the effect of variations in polyol composition over foam
 121 morphology and properties. Synthesis was carried out in a single step process and foams
 122 were cured in an open mould. Characterization was realized by optical microscopy,
 123 Fourier transform infrared spectroscopy (FTIR), thermogravimetric analysis (TGA),
 124 thermal conductivity measurements, Tapping Mode atomic force microscopy (TM-

125 AFM), Peak Force quantitative nanomechanics atomic force microscopy (PFQNM-
126 AFM), mechanical testing and dynamic mechanical analysis (DMA).

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128 **2. EXPERIMENTAL**

129 2.1. Raw materials and synthesis

130 A series of flexible polyurethane foams with variations in polyol mixture composition
131 were synthesized with castor oil based Lupranol Balance® 50 polyether polyol, kindly
132 supplied by BASF, and polytrimethylene ether glycol (PO3G) obtained from corn sucrose
133 (Ugarte et al., 2014). Amine catalyst Tegoamin® B75 and tin catalyst Kosmos® 29,
134 together with surfactant Tegostab® B-4900 (all three from Evonik) and distilled water as
135 blowing agent, were used in the B-side of the formulation. Toluene diisocyanate (TDI),
136 generously supplied by Bayer, was used as diisocyanate in the A-side of the formulation.
137 Hydroxyl number of Lupranol Balance® 50 and PO3G were determined by titration
138 according to ASTM D 4274-05. All reactants were used as received. Polyols main
139 properties are summarized in [Table 1](#).

140 Foams were synthesized at room temperature by reacting A-side with B-side in a two-
141 step reaction. Polyol or polyols mixture, catalysts, water and surfactant were mixed at
142 2000 rpm for 2 min. Then, the fixed amount of TDI was incorporated and mixing
143 continued for 10 s at the same speed. The mixture was then quickly poured into an open
144 mould to left the foam rise freely. Foams were cured at room temperature for at least 24
145 h before characterization. Isocyanate index was maintained constant (I.I.=120) in all
146 foams. Maximum PO3G substitution was 20%. With higher substitution values, foaming
147 and gelling reactions were not well balanced with the fixed catalysts quantities and the
148 obtained foams were not acceptable.

149 Foam designation and formulations are indicated in [Table 2](#).

150 2.2. Characterization techniques

151 *Cell size and density*

152 Core density of samples was determined according to ASTM D-3574-11, test A. Four
153 measurements were made for each sample. Cell size of foams was analyzed by a Nikon
154 Eclipse E 600 optical microscope. Twenty-five measurements of cell average diameter
155 were made on each sample, using a 50 magnification lens.

156 *Fourier transform infrared spectroscopy*

157 Attenuated total reflectance Fourier transform infrared spectroscopy (ATR-FTIR) was
158 used to characterize the functional groups of the synthesized polyurethane foams.
159 Measurements were performed with a Nicolet Nexus FTIR spectrometer equipped with a
160 MKII Golden Gate accessory, Specac, with diamond crystal as ATR element at a nominal
161 incidence angle of 45° with a ZnSe lens. Single-beam spectra of the samples were
162 obtained after averaging 64 scans in the range from 4000 to 800 cm⁻¹ with a resolution of
163 4 cm⁻¹. All spectra were obtained in the transmittance mode.

164 *Thermogravimetric analysis*

165 Analysis was performed on a TGA/SDTA 851 Metler Toledo equipment to evaluate
166 thermal stability of polyurethane foams. Samples were heated from room temperature to
167 650 °C at a heating rate of 10 °C min⁻¹ under a nitrogen atmosphere. For comparison
168 purposes, a foam with the same formulation to PF-100 but based on a petrochemical
169 polyether polyol supplied by Repsol and named PF-PC, was also analyzed. It had an
170 equivalent molecular weight of 1167 g eq⁻¹ and a hydroxyl number of 48 mg KOH g⁻¹.
171 The formulation of PF-PC was adjusted in order to have similar cell size and density
172 characteristics to PF-100-foam.

173 *Thermal conductivity*

174 Thermal conductivity measurements were carried out in a PVT 100 Haake equipment
175 with a 556-1082 sensor model at 35 °C. Cylindrical-shaped foam samples with a diameter
176 of 9 mm were prepared and sensor voltage was set at 2.5 V. As data deviation was very
177 low, two measurements were made for each sample.

178 *Atomic Force Microscopy*

179 Microstructure of cell struts was analyzed by TM-AFM. For specimen preparation, small
180 pieces of foam were put in silicone rubber moulds and they were filled with a low-
181 viscosity epoxy mixture. The air entrapped inside foams was removed by applying low
182 vacuum before curing the epoxy at 60 °C for 24 h. Specimens were cut with a Leica EM
183 FC6 cryo-ultramicrotome equipped with a diamond knife and operated at -120 °C. Images
184 were obtained in Tapping Mode at room temperature with a Nanoscope IIIa scanning
185 probe microscope (MultimodeTM Digital Instruments), using an integrated force

186 generated by cantilever/silicon probes, applying a resonance frequency of *ca* 180 kHz.
187 The cantilevers were 125 Nm long, with a tip radius of 5-10 nm. Morphological and
188 quantitative nanomechanical properties of foam cell struts were also analyzed by
189 PFQNM-AFM using the epoxy embed foam samples. Since the indentations occurring
190 during tip-sample interaction are in nano dimensions, the possible reinforcement effect
191 caused by the epoxy over the cell walls could be neglected. Measurements were carried
192 out using a Bruker Dimension Icon AFM operated under Peak Force mode. High
193 resolution mapping of elastic modulus was performed under room conditions with an
194 integrated TAP 150A tip having a resonance frequency of 142-162 kHz, spring constant
195 of *ca.* 3.6 Nm⁻¹ and estimated tip radius of 40 nm. For comparison purposes, a foam based
196 on PF100 formulation but with 6.5 php of water (designated as PF100H) was synthesized
197 and epoxy embed, to observe differences in microstructure and nanomechanical
198 properties when increasing urea percentage in the foam.

199 *Mechanical properties*

200 Tensile properties of polyurethane foams were analyzed according to ASTM D-3574-11,
201 test E. A MTS equipment with a load cell of 250 N and pneumatic grips was used to
202 measure the modulus of elasticity, ultimate tensile strength and percentage elongation at
203 break. Tests were performed at a crosshead rate of 500 mm min⁻¹. Tensile properties were
204 averaged for at least three specimens.

205 Measurements of compression properties were carried out according to ASTM D-3574-
206 11, test C in a MTS equipment with a load cell of 10 kN and compression plates. Tests
207 were performed at a crosshead rate of 50 mm min⁻¹ and final force was determined after
208 60 s. Three specimens per sample were at least analyzed.

209 All tensile and compressive properties were measured in the foam rise direction.

210 *Dynamic mechanical analysis*

211 DMA was performed in tensile mode with an Eplexor 100 N analyzer, Gabo equipment.
212 Measurements were carried out at a scanning rate of 2 °C min⁻¹ from -100 to 200 °C, using
213 an initial strain of 2%. The operating frequency was 1 Hz. Approximate dimensions of
214 foams were 20 x 5.5 x 3.5 mm³ (length x width x thickness). DMA measurements were
215 also performed in the foam rise direction.

216 3. RESULTS AND DISCUSSION

217 3.1. Density and cell size

218 Density measurement results are shown in Table 3. Cellular structure and cell size of the
219 foams were observed by optical microscopy (Fig. 1) and cell size values are also resumed
220 in Table 3. It was observed that density decreased when increasing PO3G content until a
221 10% substitution, and then increased. The same tendency was observed by Tu et al., 2008
222 when substituting a petrochemical polyol with epoxidized soybean oil with higher
223 hydroxyl number. Lim et al., 2008 analyzed the effect of polyol hydroxyl number in
224 polyurethane foam formulations. They also observed that when increasing hydroxyl
225 number while maintaining isocyanate index constant, the density reached a minimum and
226 then increased. It was concluded that the decrease of the molecular weight when
227 increasing hydroxyl number caused a better mobility of the mixture and the blowing
228 efficiency increased. Upon the minimum value, the increase of viscosity due to the
229 intensive formation of allophanate and biuret crosslinks is believed to hinder foaming
230 reactions. Moreover, the increased reactivity of highest PO3G substitution polyol
231 mixtures may have fastened the gelling reaction and the cell structure became strong
232 enough before it was blown (Kang et al., 2012) keeping the cell size small.

233 PF90 had the lowest density and the highest cell anisotropy as well as one of the highest
234 cell sizes. Cell size results showed a direct relationship with foam density. Foams with
235 the highest density had the smallest cell sizes and lowest cell anisotropy. PF100 and PF80
236 showed very similar structures.

237 3.2. FTIR

238 ATR-FTIR results of polyurethane foams ranging from 100% to 80% Lupranol Balance®
239 50 polyol showed transmittance bands corresponding to both main reactions taking place
240 in polyurethane foam chemistry: urethane and urea bonds. As shown in Fig. 2, all spectra
241 were quite similar but slight differences due to polyol composition were observed.

242 Transmittances at wavenumbers 1223 cm^{-1} and 1730 cm^{-1} were assigned to the ester
243 asymmetric absorbance and the ester carbonyl absorbance (Singhal et al., 2014),
244 respectively. It was observed that as the Lupranol Balance® 50 content in the foam
245 formulation decreased, ester carbonyl absorbance peak intensity diminished due to the
246 incorporation of ether groups in the formulation instead of ester groups.

247 In the amide I region, the bands corresponding to free C=O stretching of urea (around
248 1715 cm^{-1}) and urethane (around 1730 cm^{-1}) were observed (Elwell et al., 1996). The
249 deconvolution of the observed peak allowed calculating the relative areas corresponding
250 to each type of stretching. An example of the deconvolution is shown in Fig. 3.

251 The area and the wavenumber (WN) corresponding to each peak are summarized in Table
252 4.

253 As PO3G content increased, shifts to lower wavenumbers were observed for both free
254 urea and free urethane stretching vibration and the total area also diminished. On the same
255 fashion, urea/urethane ratio value diminished as PO3G content increased. Results suggest
256 that as PO3G is incorporated in the formulation, ureas may be able to form ordered
257 domains as less free urea groups were observed by ATR-FTIR analysis.

258 The transmittance band at 1640 cm^{-1} corresponds to bidentate (hydrogen bonded) urea
259 and could be used as an identification of ordered hard domains (Heintz et al., 2005). As
260 a general tendency, it was observed that foams with the highest quantity of PO3G in the
261 formulation showed the most intense peaks. The results agree with the deconvolution
262 analysis, indicating the formation of more ordered urea domains as the short glycol is
263 incorporated in the formulation.

264 3.3. Thermal properties

265 Thermal degradation properties of polyurethane foams are essential regarding a safe use.
266 In this way, the thermal degradation behavior of bio-based polyurethane foams was
267 compared with a petrochemical polyol based foam. Thermograms of polyurethane foams
268 under nitrogen atmosphere are shown in Fig. 4. Petrochemical polyol based foam
269 maintained stable until $200\text{ }^{\circ}\text{C}$, while bio-based polyurethane foams started degradation
270 around $220\text{ }^{\circ}\text{C}$. Results showed that degradation occurred in two steps. The first step was
271 assigned to degradation of urea and urethane linkages (Ravey et al., 1997). According to
272 first derivative thermogravimetric (DTG) curve, the maximum urea and urethane
273 degradation rate for the petrochemical polyol based foam and bio-based foams were
274 detected at $290\text{ }^{\circ}\text{C}$ and $300\text{ }^{\circ}\text{C}$ respectively. The second step corresponds to polyol
275 degradation (Allan et al., 2013). Analyzing the maximum degradation rate temperature,
276 bio-based polyols conferred enhanced thermal stability ($400\text{ }^{\circ}\text{C}$) comparing with

277 petrochemical polyether polyol (377 °C). Char formation was negligible in all cases, with
278 a maximum of 2.3% for PF100 foam.

279 Thermal conductivity values of foams were very similar with an average of 0.069 W m⁻¹
280 K⁻¹, indicating that they all have similar open-closed cell proportions. Values were quite
281 high comparing with other data reported in literature for foams obtained from both
282 vegetable oil based polyols and petrochemical polyols (Badri et al., 2012; Jeong et al.,
283 2009). This could be due to the foam disposition during the analysis, which could be
284 slightly compressed by the temperature probe.

285 3.4. Foam strut morphology and elastic modulus

286 TM-AFM was used to obtain phase images of PF100 and PF80 polyurethane foams (Fig.
287 5). High dissipating soft phases give dark contrast while rigid phases are identified as
288 bright areas. More rigid (Yilgor et al., 2007), urea rich regions may appear brighter than
289 polyol soft regions (Aneja et al., 2002). On the analyzed figures, microphase segregation
290 of different phases was observed (Lan et al., 2011) with bright regions dispersed in a dark
291 continuous phase. According to relative dissipation energies, it was concluded that bright
292 regions correspond to urea rich domains dispersed in polyol rich domains. In PF80
293 sample, soft polyol domains seemed to be purer since in PF100 sample more small bright
294 crystals were observed dispersed in soft domains. Comparing PF100 and PF100H
295 samples, it could be said that in PF100H, the urea hard domains create a more
296 interconnected network across the continuous soft domain.

297 Topographic and elastic modulus mapping images obtained with PFQNM-AFM are
298 shown in Fig. 6. Represented elastic modulus profiles were randomly selected from dark,
299 low modulus areas. To obtain an average modulus value of such regions, six profiles were
300 extracted and the average value was calculated on each sample. Results together with
301 sample roughness are summarized in Table 5.

302 On elastic modulus mapping images, bright areas with high modulus were clearly
303 distinguished from low modulus dark regions. Given that polyureas are more rigid than
304 polyurethanes (Yilgor et al., 2007), it might be determined that bright areas correspond
305 to urea rich domains. Taking this into account, the images are in accordance with TM-
306 AFM phase images, where urea rich domains appear dispersed in a soft segment rich
307 matrix. Modulus values were quite in accordance with previous works. For instance,

308 Schön et al., 2011 used Peak Force Quantitative Nano-Mechanics equipment to
309 characterize the elastic modulus of segmented thermoplastic polyurethanes. Obtained
310 modulus values were of the same order of magnitude although those of foams were
311 higher. The increase of modulus on foams was attributed to the urea domains dispersed
312 in the soft domains. The decrease in modulus from PF100 to PF80 could indicate a better
313 phase separation as PO3G is introduced in the formulation. A purer soft phase involved
314 a lower number of urea domains dispersed in the polyol rich phase and this may have
315 lowered the average modulus of the soft phase in PF80 sample. This result was in
316 accordance with FTIR analysis. PF100H sample showed the lowest modulus in dark
317 phases, suggesting that the increased urea quantity on this foam favored their association
318 and thus phase separation was enhanced. Roughness values increased both as PO3G was
319 eliminated from polyol composition and more water was incorporated in the formulation.

320 3.5. Mechanical properties

321 Results concerning tensile strength, elastic modulus and ultimate elongation are shown in
322 Fig. 7.

323 Tensile properties showed a very similar behavior to density and cell size. As a general
324 tendency, it was observed that as foam density increased and cell size decreased, tensile
325 behavior enhanced. PF90 showed the poorest tensile properties, the foam with highest
326 cell size and one of the highest cell anisotropy. Compression force deflection (CFD)
327 value results are shown in Fig. 8. According to Tu et al., 2008, compressive properties of
328 foams seem to be influenced by both density and crosslinking density. On synthesized
329 series, as PO3G has higher hydroxyl value than Lupranol Balance[®] 50, the number of
330 equivalent OH groups increased with the incorporation of PO3G to the formulation. Since
331 isocyanate index was maintained constant in all samples, the quantity of NCO groups in
332 the foam increased with the addition of PO3G. It seemed that until 10% of PO3G
333 substitution, the effect of density decrease overlapped crosslinking effect and CFD values
334 were not enhanced. However, in foams with high PO3G substitution, both density and
335 crosslinking density increased and compressive properties increased, especially in PF80
336 sample.

337 3.6. Dynamic mechanical properties

338 The evolution of storage modulus and $\tan \delta$ values with temperature was analyzed by
339 DMA (Fig. 9). Storage modulus showed two plateau regions, the one at low temperatures
340 corresponding to glassy state and the one at high temperatures corresponding to rubbery
341 state of the foam. Obtained values were quite similar, however, the porous nature of the
342 foams made very difficult to measure the real area and hence to obtain reliable modulus
343 values (Das et al., 2009). This drawback is avoided in $\tan \delta$ analysis since values are not
344 influenced by the sample area. According to storage modulus evolution, samples showed
345 a single $\tan \delta$ peak at around - 40 °C, corresponding to the beginning of molecular motions
346 in the polyol chains. Results were similar to other works with bio-based polyols (Das et
347 al., 2009; Sonnenschein et al., 2013; Tu et al., 2009). As a general tendency, glass
348 transition temperature values slightly shifted to lower temperatures as PO3G was
349 incorporated to the polyol mixture.

350

351 **4. CONCLUSIONS**

352 Bio-based polyols showed to be good candidates for being used in flexible polyurethane
353 foam synthesis. Foams with polyol mixtures ranging from 100% castor oil based
354 Lupranol Balance[®] to 20% of PO3G substitution were successfully synthesized by a one
355 shot method in an open mould. Foams with an open celled structure and acceptable
356 densities were obtained. Results indicated that the incorporation of PO3G in the
357 formulation favoured hydrogen bonding between urea groups, suggesting that phase
358 separation was enhanced. Bio-based foams showed improved thermal stability, with no
359 significant mass loss until 220 °C. Morphological analysis of foam struts revealed the
360 existence of a phase separated structure. Nanomechanical properties of different phases
361 were measured by Peak Force quantitative nanomechanics AFM and results were
362 satisfactorily used to asses phase separation in polyurethane foam strut. Observations
363 suggested that phase separation was enhanced when incorporating PO3G in the polyol
364 formulation. Polyol composition was believed to alter the reactivity and obtained three-
365 dimensional structures, thus affecting mechanical properties of the foams.

366

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- 483

484 **Table 1.** Main properties of the polyols.

Property	Lupranol Balance® 50	PO3G
OH number (mg KOH g ⁻¹)	49.7	79.4
Functionality	2.7	2
Number average molecular weight (g mol ⁻¹)	3048	1413

485

486 **Table 2.** Designation and formulation of synthesized polyurethane foams (PF). All formulations are based
487 on 100 parts by weight of polyol (php).

Component	PF100	PF95	PF90	PF85	PF80
Lupranol Balance®50	100	95	90	85	80
PO3G	-	5	10	15	20
Water	3.5	3.5	3.5	3.5	3.5
Tegoamin®B75	0.3	0.3	0.3	0.3	0.3
Kosmos® 29	0.4	0.4	0.4	0.4	0.4
Tegostab® B-4900	1.1	1.1	1.1	1.1	1.1
TDI (g)	49.3	49.6	50.0	50.3	50.6

488

489 **Table 3.** Density and cell size of synthesized foams.

Sample	Density (kg m ⁻³)	Cell size (µm)
PF100	42.00 ± 0.97	263.29 ± 74.21
PF95	40.65 ± 0.97	252.77 ± 114.32
PF90	38.55 ± 0.54	287.54 ± 150.24
PF85	39.20 ± 0.65	322.89 ± 143.28
PF80	42.35 ± 0.94	275.39 ± 103.47

490

491 **Table 4.** Analysis of free urethane and free urea areas for PF100, PF90 and PF80 samples.

Sample	Free urethane		Free urea		R
	Area	WN	Area	WN	Urea/Urethane
PF100	77.2	1734	267.8	1716	3.5
PF90	89.8	1733	145.0	1715	1.6
PF80	108.1	1731	101.9	1712	0.9

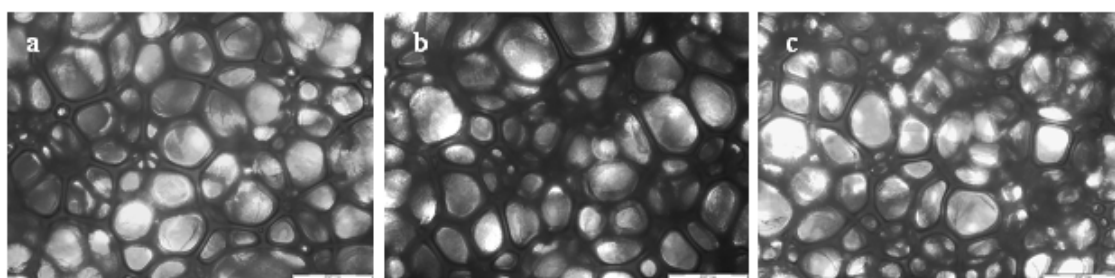
492 **Table 5.** Roughness and elastic modulus data of PF100, PF80 and PF100H samples.

Sample	Roughness (nm)		Elastic Modulus (MPa)
	R _a ¹	R _q ²	
PF100	4.25	5.92	191 ± 44
PF80	3.18	4.07	159 ± 10
PF100H	7.58	9.54	106 ± 12

493 ¹: arithmetic average roughness

494 ²: root mean square roughness

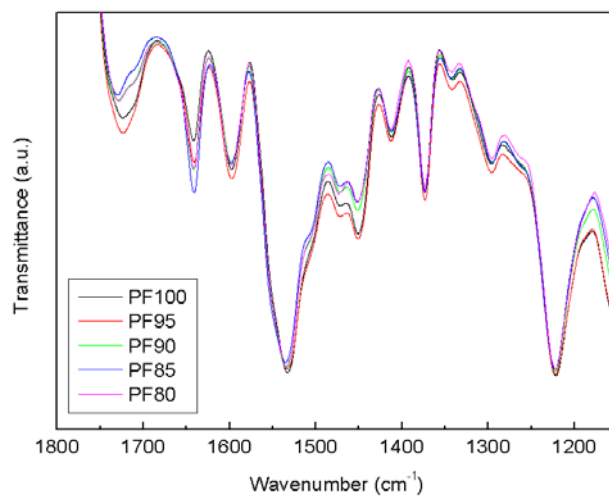
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496

497 **Fig. 1.** Optical micrographs of (a) PF100, (b) PF90 and (c) PF80 polyurethane foams
498 (scale bar: 200 μm).

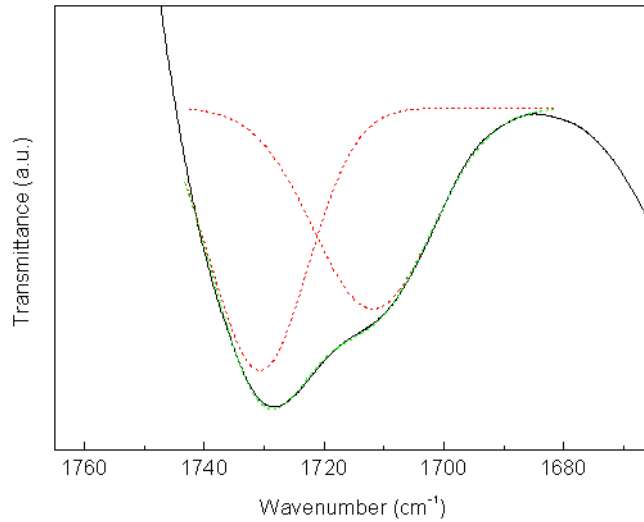
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500

501 **Fig. 2.** FTIR spectra of the synthesized foams on the range from 1800 cm⁻¹ to 1100 cm⁻¹.

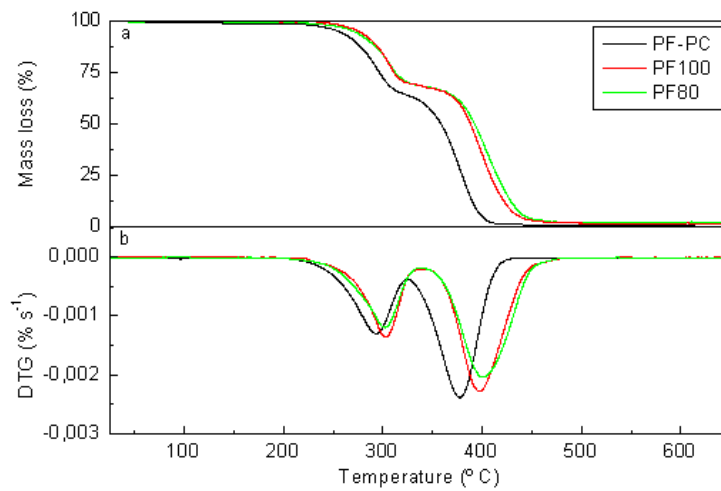
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504 **Fig. 3.** Peak deconvolution for PF80 sample.

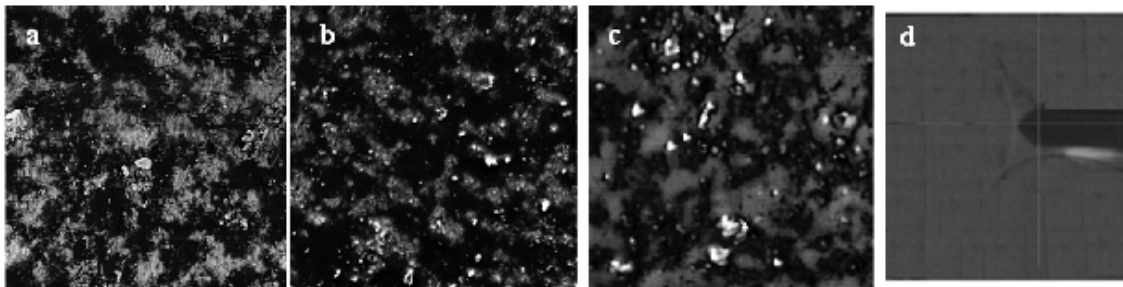
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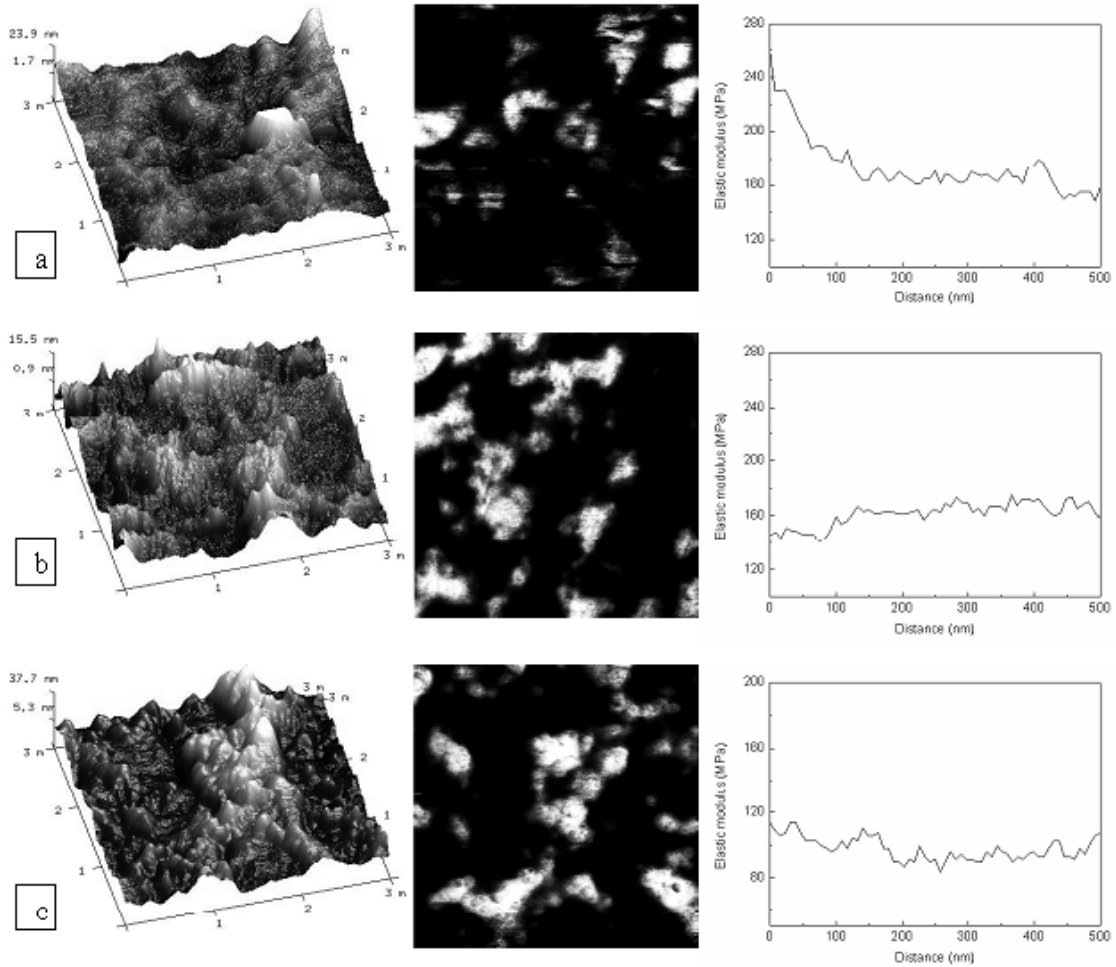
507 **Fig. 4.** (a) TGA thermograms of PF-PC, PF100 and PF80 foams and (b) DTG curves of
508 PF-PC, PF100 and PF80 foams.

509



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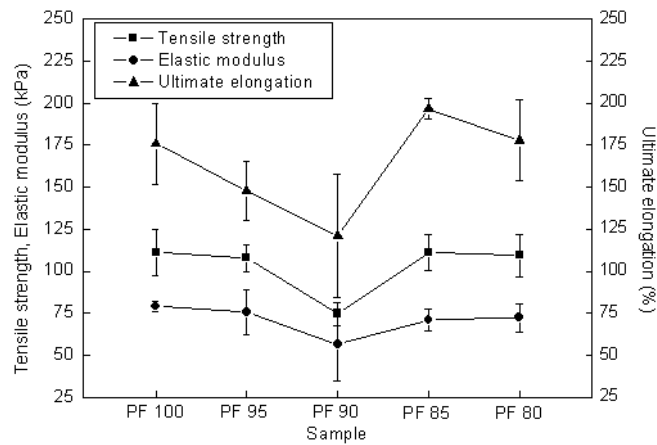
511 **Fig. 5.** AFM 5x5 μm² Tapping Mode phase images of (a) PF100, (b) PF80, and (c)
512 PF100H and (d) positioning of AFM tip on cell strut.



513

514 **Fig. 6.** AFM topographic 3D $3 \times 3 \mu\text{m}^2$ images (left), elastic modulus $3 \times 3 \mu\text{m}^2$ images
 515 (center) and cross-sectional elastic modulus profiles (right) of (a) PF100, (b) PF80 and
 516 (c) PF100H samples obtained from PFQNM-AFM.

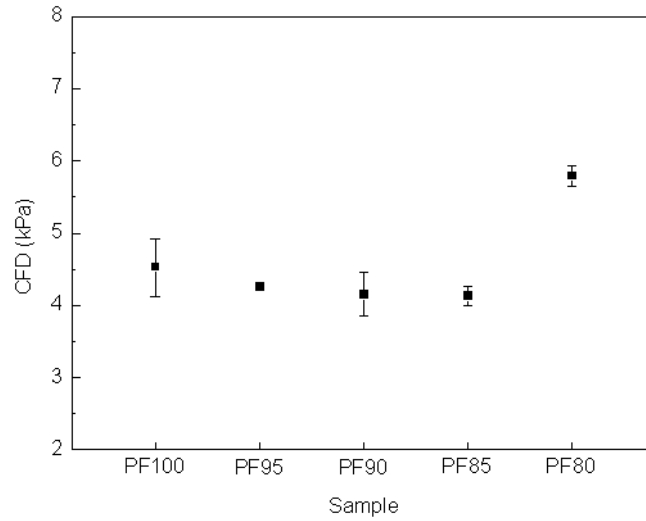
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519 **Fig. 7.** Tensile strength (■), elastic modulus (●) and ultimate elongation (▲) of
 520 synthesized samples.

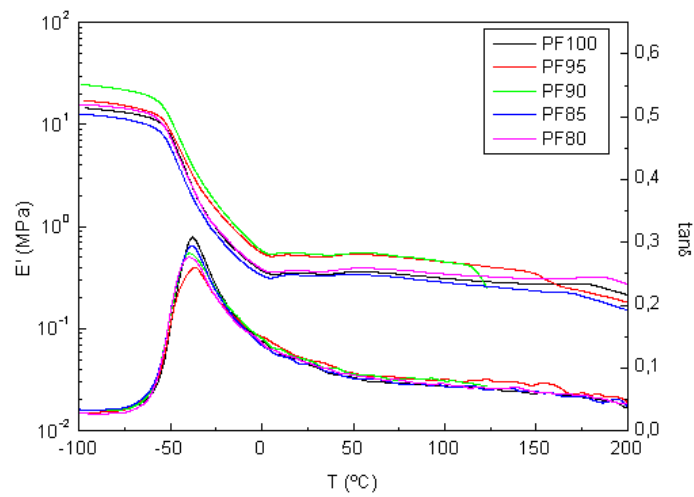
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523 **Fig. 8.** CFD values of synthesized foams.

524



525

526 **Fig. 9.** Storage modulus (E') and $\tan\delta$ as a function of temperature for synthesized foams.